

## 80751 PFC BOOST MODULE SERIES

### Application Information

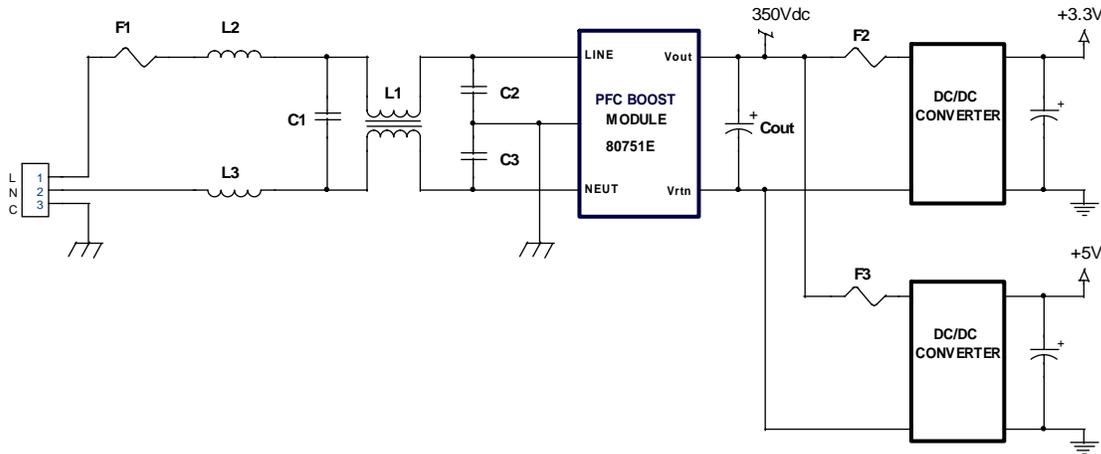


Figure 1. Typical Application Circuit, 3.3V & 5V, 60W Combined Output Power

| Designator | P/N or Description              |
|------------|---------------------------------|
| F1         | 2A, 125Vac, Fast-Blow           |
| F2, F3     | 2.5A, 450V, PC-Tron             |
| L1         | 6.8mH, 1.5A, Schaffer or Equiv. |
| L2, L3     | 330uH, Coilcraft #DO5022-334    |
| C1         | 0.047uF, 275Vac, "X2"           |
| C2, C3     | 3300pF, 250Vac, "Y1/Y2"         |
| IC1        | PPI p/n 80751                   |
| IC2        | COTS HV DC/DC Converter         |
| IC3        | COTS HV DC/DC Converter         |

#### OVERVIEW:

Implementing power factor correction (PFC) into switch mode power supplies maximizes the power handling capability of the power supply and current handling capacities of power distribution networks. Input power factor (PF) is defined as real power (Watts) divided by apparent power (VA) and is expressed as decimal number between 0 and 1. A non-corrected power supply with a typical PF equal to 0.65 will draw approximately 1.5 times greater input current as a PFC supply (PF=0.99) for the same output loading. The non-corrected supply requires additional AC current to be generated which is not consumed by the load, creating  $I^2R$  losses in the power distribution network.

Ideally, PFC power supplies "look" like a resistor to the driving voltage source; the current drawn by the supply matches the voltage in waveshape and phase. Power factor will approach unity when the input current drawn by the power supply matches and is in phase with the input voltage. For a sine wave voltage source, the input current of a well designed PFC supply will also be a sine wave. A perfect sine wave contains no harmonic distortion (all individual higher order harmonics have zero magnitude). As a result, a derivative of active power factor corrected power supplies, when subjected to a non-distorted input source, is minimization of input current harmonic distortion content.

Airborne equipment must comply with stringent standards regarding input power factor and input current harmonic distortion content. RTCA/DO160D section 16 and Boeing's D6-44588 require minimization of individual harmonic distortion content up to the 40<sup>th</sup> harmonic (2kHz at 400Hz fundamental frequency) for all equipment that draws more than 35VA. Limits set forth in these specifications mandate active PFC correction for most airborne equipment power supplies. For a non-distorted single phase AC voltage source, individual input current harmonic distortion requirements are:

| Harmonic Order   | Limits                |
|--|-----------------------|
| Odd triplen harmonics;<br>(h = 3, 9, 15, 21, 27, 33, 39)                         | $I_h = 0.15(I_f) / h$ |
| Odd non triplen harmonics;<br>(h = 5, 7, 11, 13, 17, 19, 23, 25, 29, 31, 35, 37) | $I_h = 0.3(I_f) / h$  |
| Even harmonics 2 & 4;<br>(h = 2 and 4)   | $I_h = 0.01(I_f) / h$ |
| Even harmonics > 4;<br>(h = 6, 8, ... 40)  | $I_h = 0.0025 (I_f)$  |

Where:

h = order of harmonic

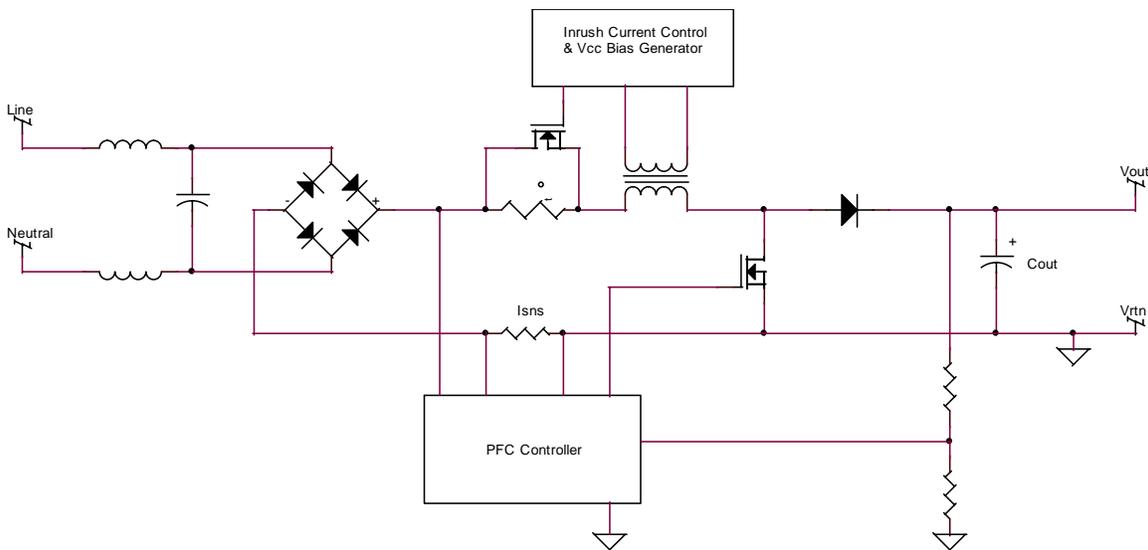
$I_h$  = maximum harmonic current of order h obtained during min, max and steady state operation

$I_f$  = fundamental current obtained during min, max and steady state operation

Individual harmonic currents < 5mArms are disregarded (<10mArms for DO160F)

Recently, requirements have been added to these specifications that require test and compliance with input harmonic distortion for variable frequency generators from the minimum input line frequency of 360Hz through the maximum input line frequency of 800Hz.

A block diagram of an active PFC boost converter is shown in figure 2. The input stage of this type of converter is the same as a conventional non-corrected power supply; the input AC is filtered and rectified. In order to boost the output and to control the input current, the large input capacitor that would normally be associated with the AC to DC conversion function has been moved to the output of the boost converter;  $C_{out}$  in the diagram. The PFC controller circuitry programs the input current to track the input voltage by varying the main MOSFET duty cycle based on two feedback and one feedforward signals: output voltage, rectified line current and rectified AC voltage. The output of the boost regulator is a constant voltage but the input current is programmed to be a half sine wave. The power flow into  $C_{out}$  is a sine wave at twice the line frequency.



## APPLICATION CIRCUIT

A schematic of a typical PFC, dual output 3.3V and 5V modular power supply is provided in figure 1. A modular supply of this type is practical for one, two or three outputs and can accommodate any isolated output voltage from 2V to 48V. There are a variety of compatible DC/DC converters available off the shelf that can operate from a 350Vdc bus. The downstream DC/DC converters must be capable of operating from a high voltage input, typically between 180Vdc and 400Vdc. As the number of outputs is increased beyond three, it is often times more cost effective and space effective to incorporate a discrete power supply.

When configured properly, the PFC modular supply depicted in figure 1 will operate from a 115Vrms, single phase, 47Hz – 800Hz input source and will provide approximately 60W combined output power. Provided

sufficient output hold-up capacitance ( $C_{out}$ ) is incorporated, the supply will comply with all of the input power requirements per RTCA/DO-160D, section 16 for the wide variable frequency category A(WF). This includes normal and abnormal operating conditions for AC equipment as well as the A(WF) limits for input harmonic distortion.

Supply hold-up time is selectable by implementation of high voltage electrolytic capacitors ( $C_{out}$ ) connected at the output terminals of the PFC converter module. For applications requiring higher output power levels, the PFC converter module can be substituted for one offering higher power capacity.

## COMPONENT SELECTION:

### EXTERNAL EMI FILTER

An external common-mode filter (L1, C2 & C3) is necessary when implementing the 80751 series PFC boost module into a modular supply for compliance with RTCA/DO-160D conducted emissions requirements. The common-mode filter shown in the application circuit above, in cascade with the normal-mode filter internal to the 80751 module, will suppress conducted emissions to levels below DO-160D requirements. The differential filter shown comprising of L2, L3 and C1 is provisional and is included in order to gain additional margin in the normal mode. The external filter should be placed as close as possible to the AC entry point within assembly (i.e., at the power connector). The addition of L1, C2 and C3 will have minimal impact on harmonic distortion performance of the 80751 boost module. The differential filter comprised of L2, L3 and C1 will have an adverse effect on harmonic distortion and the value of C1 needs to be kept small (on the order of 0.047 $\mu$ F per 50W of input power) in order to minimize the impact on individual harmonic distortion levels when subjecting the supply to input voltage distortion greater than 5% ( $V_{thd}$ ), particularly at 800Hz. The configured modular supply with external filter should be evaluated for harmonic and emissions performance within the application prior to finalizing component values.

#### Common Mode Choke -Suggested Manufacturers:

Shaffner EMC, Inc  
www.schaffner.com  
RN214 series

Coilcraft  
www.coilcraft.com  
CM3595 series

### OUTPUT CAPACITOR(S) ( $C_{out}$ )

The 80751 PFC boost converter requires a minimum output capacitance of 100 $\mu$ F for proper module operation. Typical values will be larger due to the hold-up time requirements of the particular application. If loading the output of the converter, a minimum of 100 $\mu$ F of output capacitance must be established through a low impedance connection to the output terminals of the module or the module's output will not regulate properly. Failure to maintain this minimum capacitance while loading the output can result in permanent damage to the 80751 module.

The 80751 module's maximum allowable output capacitance is 1000 $\mu$ F. If exceeding this value, proper module start-up during full load at low input line may be compromised and should be verified. When incorporating larger values of output capacitors and using DC/DC converters that turn-on at voltages well below the module's rated output voltage, verify proper modular supply start-up at low line input voltages. The module's output power limit set point (~95W $_{out}$ ) can be exceeded due to the combination of charging the output capacitor bank and driving the DC/DC converter load causing cyclic on/off of the boost module when starting at low line. This condition can be corrected by delaying the DC/DC converter at start-up until the boost module is at or near its specified output voltage, or selecting a higher power front-end boost converter module.

#### Recommended Hold-up Capacitor Type and Placement:

- United Chemi-Con, KMH series, 450V, 105°C, Snap-mount
- Nichicon, GJ(15) Series, 400V, 105°C, Snap-mount, 15mm height

#### Placement:

Output capacitor(s) should be placed within several inches of the boost module output prior to the DC/DC converter input fuses, F2 and F3.

#### Output Capacitor Ripple Requirements:

Observe capacitor ripple current requirements at 800Hz and 100kHz (when operating at 400Hz input frequency). Normal full load 800Hz ripple current can be approximated by:

$$I_{800} \sim P_{in} / V_{in} \text{ (rms)}$$

100kHz ripple current content is generated as a function of the boost module's normal operation. The maximum 100kHz ripple current for the 80751 series is 500mA<sub>pk-pk</sub> and occurs at the internal switching frequency of the converter.

#### Hold-up Time Calculations:

Output capacitance (C<sub>out</sub>) vs. hold-up time (t) can be calculated by the following formula:

$$E = Pt = 1/2C_{out}(V_i^2 - V_f^2)$$

where:

P = Power delivered to DC/DC converters

V<sub>i</sub> = Normal operating DC output voltage of boost converter (350Vdc)

V<sub>f</sub> = Minimum operating voltage of DC/DC converter

#### FUSES

Properly fusing the input line is necessary for safeguarding against a catastrophic failure within the input filter capacitors, the 80751 boost module, the output electrolytic capacitors (C<sub>out</sub>) or the DC/DC converters. The 80751 PFC boost module does not contain overcurrent protection; if a short circuit or low impedance condition is applied across its output terminals, there is no internal current limiting feature. The topology of a boost converter (see figure 2) is such that it resorts back to a standard rectifier/ bulk capacitor front-end when the boost function is inhibited. For this reason, without implementing elaborate current sensing and protection circuitry in the rectified line, the boost converter is inherently not protected against shorted or low impedance output conditions.

Fusing the DC/DC converter input lines is necessary for safeguarding against a catastrophic DC/DC converter failure. Although the input line fuse will eventually activate, DC fuses positioned right at the input to the DC/DC converters will limit the energy delivered by the hold-up capacitors (C<sub>out</sub>) and will prevent secondary overcurrent stress and/or failure to the PFC boost module.

Fuse charts (I versus t) should be examined to verify that the line fuse selected will not prematurely activate as a result of normal inrush currents flowing at supply start-up. Inrush current is limited within the 80751 module to 5A<sub>pk</sub> (3.54A<sub>rms</sub>) by an active inrush current limiting circuit. Inrush current duration (t) increases with increasing output capacitance (C<sub>out</sub>) and can be approximated by  $t = (50) \times (C_{out})$ .

F1 = 2A, 125Vac, Fast-Blow

F2 = F3 = Bussmann, PC-Tron, DC Fuse, PCB Series, 450V/2.5A

#### EMI CONSIDERATIONS

Certain measures should be taken to assure successful EMI compliance. Among these are:

- Use of solid chassis ground plane on power supply PCB
- Solid mechanical interconnection from chassis ground to module frame (#4 hardware, 4 places)
- Incorporation of suggested common mode choke (L1) and filter capacitors (C1, C2 & C3)
- Observance of EMI guidelines for specific DC/DC converters chosen
- Avoidance of routing traces directly under module

## EFFICIENCY & POWER CONSUMPTION

Typical efficiency for the 80751 converter module is 88%. For maximum output power of 75W, the 80751 will consume approximately 10W. Quiescent power consumption is 3.5W (at no output load). When determining 80751 temperature rise, power consumption can be calculated or measured and multiplied by the thermal resistance from module baseplate to ambient. See the thermal table in the 80751 data sheet for coefficients versus airflow.

When computing overall modular power supply efficiency the boost converter efficiency must be multiplied by the downstream DC/DC converter efficiencies. When computing energy requirements for the hold-up capacitors, only the efficiency of the DC/DC converters needs to be considered.

The 80751 contains an internal power limit feature to assure the module's internal switching (power stage) circuitry is not overstressed when load demands are higher than the module's rated output power. The power limit set-point is approximately 95W. Load demands exceeding this value will cause the module's output voltage to foldback; the internal boost converter duty cycle will reduce proportional to the overload demand in order to keep the output power constant and limited. This feature does not safeguard against a shorted output – the input line must be properly fused to protect the module's internal bridge rectifier and AC current sensing circuitry.

## PRECAUTIONS

### ISOLATION

The 80751 PFC boost module is a non-isolated device. The output is a 350Vdc differential potential but not with respect to chassis ground. The 350V return line (Vrtn) is not at chassis potential. Isolation (primary to secondary) is accomplished within the DC/DC converters. Special care must be exercised when monitoring the module's DC output on an oscilloscope. Either the oscilloscope must be floated from chassis ground or the input neutral line disconnected from chassis ground. Typical aircraft application is to tie neutral and chassis ground together. Failure to isolate neutral from the module's return line can permanently damage the boost module device. Proper input fusing of the AC high line should protect the boost module in the event the neutral is inadvertently tied to the module's return line (i.e., during testing).

### PRIMARY TO SECONDARY ISOLATION

Primary to secondary isolation for the configured supply is achieved within the DC/DC converters. Typically, the level of isolation provided within the DC/DC converter is more than sufficient for airborne applications; airborne specifications require 1500Vrms primary to secondary isolation. It is imperative from a safety standpoint to avoid commingling input AC referenced circuitry from DC output secondary referenced circuitry. A general guideline is to maintain at least 4mm creepage/clearance distance between any primary referenced circuit and any secondary referenced circuit.

### THERMAL CONSIDERATIONS

The maximum baseplate temperature rating for the 80751 module is 100°C. There is no derating required; the module can supply full output power up to the maximum baseplate temperature. The modules contain overtemperature protection, it is activated at a sensed baseplate temperature exceeding 100°C. When activated, the module's boost function is inhibited. During this time the module's output voltage will be ~162Vdc depending on output loading. This level is typically below the input operating threshold of the downstream DC/DC converters thus disabling all low level outputs during an overtemperature fault. Module recovery is automatic with ~20°C hysteresis.